



## General considerations for the influence of mesh density in LS Dyna

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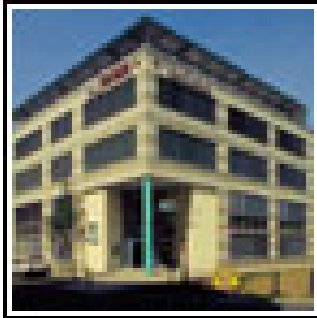
5th European LS-DYNA User Conference, Birmingham, May 2005

## **Agenda**

- Tecosim-best partner for simulation
- Introduction
- FE Experiments with varied parameters
- Analysis of Results/ Conclusion
- Automatic Meshing Pro's and Con's
- Summary

- Company Founded 1992
- Strategic CAE Partner of Major OEM's and Suppliers
- Turnover € 7,1 Mio in 2004
- Currently **75 Employees** at 5 European Locations
- State-of-the-Art IT Infrastructure
- Comprehensive liability insurance
- Quality Management System according to ISO 9001, UM 14001 and Customer Specific Requirements (FORD Q1 Award)
- Associated member of the FAT (Forschungsvereinigung Automobil Technik) research team for finite element coupling for crash calculation

# Locations & References



Rüsselsheim



Köln

- Audi AG
- Adam OPEL AG
- Claas
- Daimler Chrysler
- Daihatsu
- Fiat
- FORD
- General Motors
- HONDA
- ISUZU
- KIA
- John Deere
- Jaguar
- Landrover
- Nissan
- PORSCHE AG
- Toyota
- AMG
- Autoliv
- Bayer AG
- Bentler
- Bertone
- Bosch/ Blaupunkt
- Degussa-Hüls AG
- Dynamit Nobel
- EADS
- Faurecia
- Getrag
- Hella KG
- Johnson Controls
- Karmann
- Lear
- Magna
- Thyssenkrupp
- TRW Automotive
- Mahle
- MAN
- Mannesmann/Sachs
- Siemens VDO
- Wagon Automotive



Leonberg



Basildon (UK)



Coventry (UK)



Igenie Office  
Tokio (Japan)

- State-of-the-Art scalable NEC MPP Linux cluster (64 CPU) with short Turnaround Time for Full Car Crash Analysis
- 64 bit Numbercruncher (Itanium/Opteron) for Implicit codes
- Branches Interlinked by 2 Mbit Leased Lines
- ENX Access
- Major CAE and CAD Systems
- Development of Methods, Routines and Templates

**NEC**

## Explicit Codes

- LS-Dyna
- PAMCrash/PAMSafe
- Radioss
- Abaqus explicit

## Implicit Codes

- Nastran, Abaqus
- Ansys, Mechanical

## CFD Code

- StarCD

## Pre-/Postprocessor

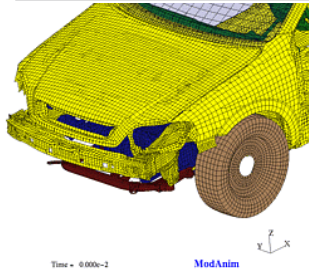
- Ansa
- HyperWorks
- Animator
- Sofy
- Medina
- Patran

## Optimisation

- OptiStruct
- HyperOpt
- HyperStudy
- I- Sight

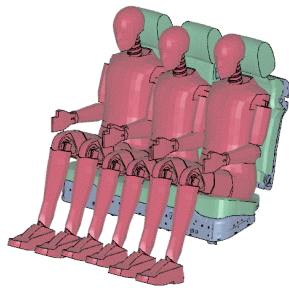
## MKS Codes

- Madymo
- Adams
- Motion solve

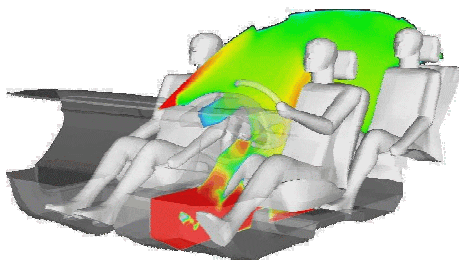


CRASH

Frontcrash  
Time= 0



Seats



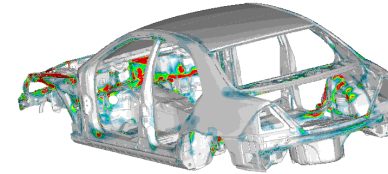
CFD



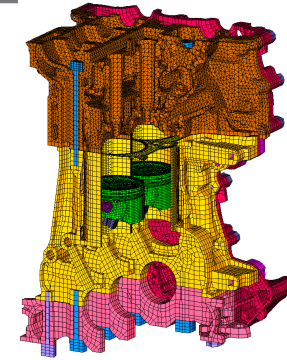
Safety

## 9. Optimization

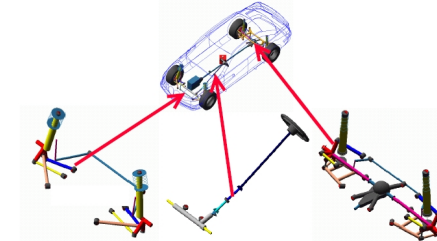
- Linear Parameter Optimization
- Non- Linear Parameter Optimization
- Design Optimization



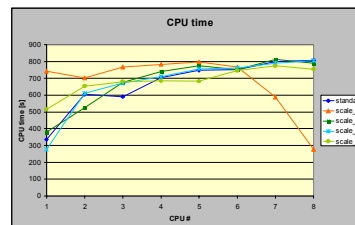
NVH / Durability



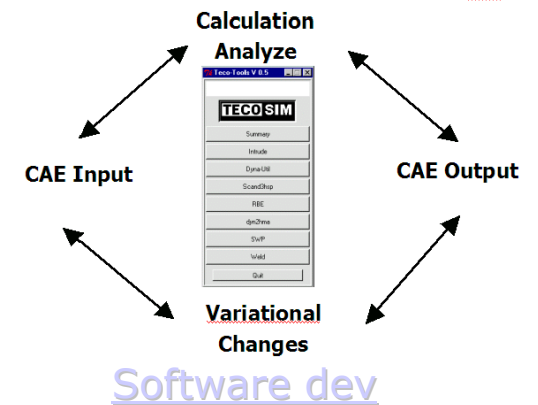
Powertrain



Multi Body Systems (MBS)



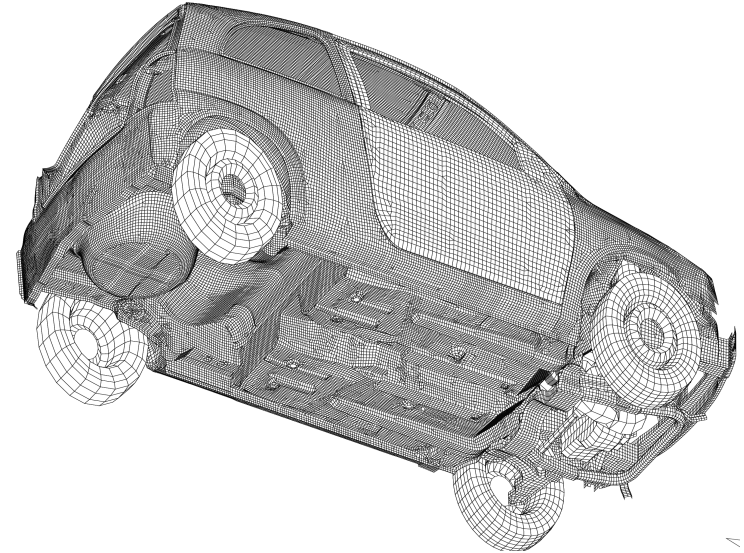
Optimization



***Any sufficiently advanced technology is indistinguishable from magic.***

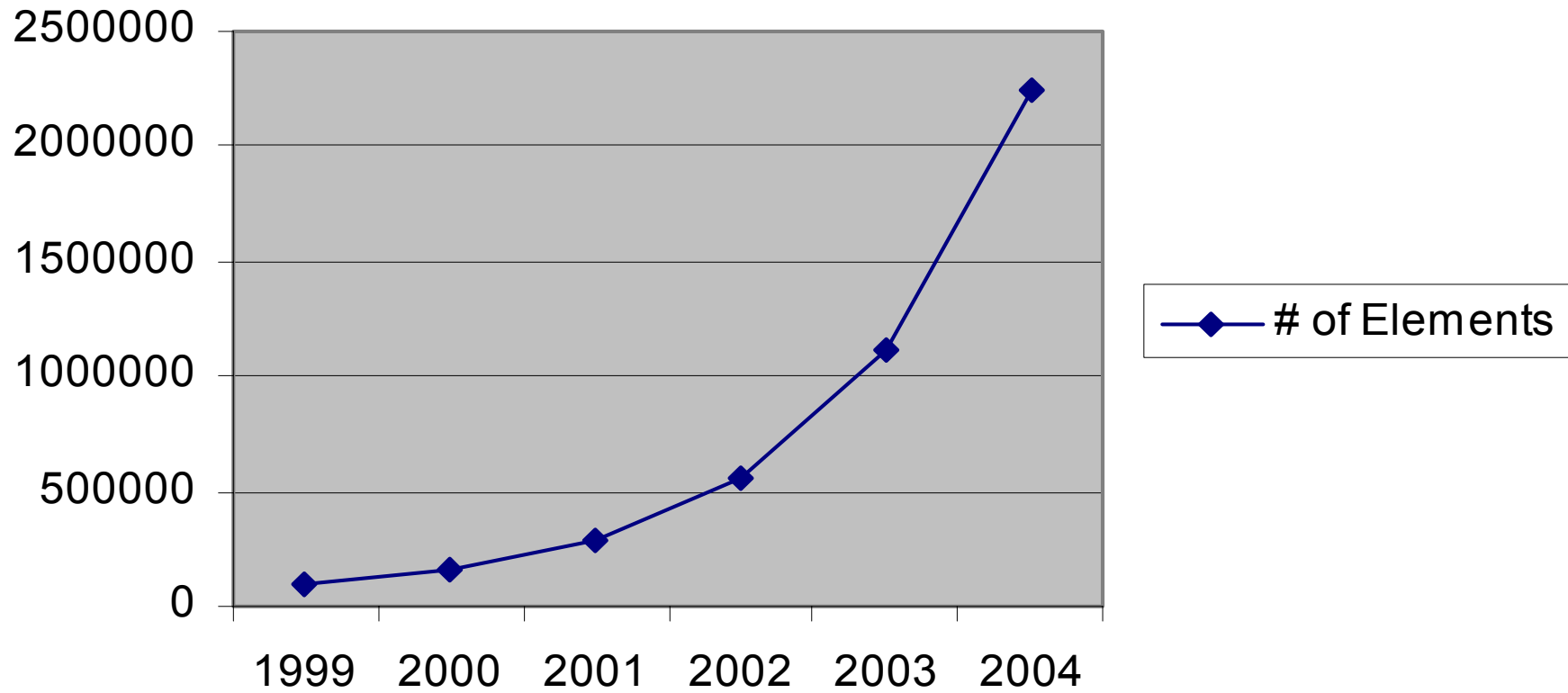
„Profiles of the future“ (1961) by Arthur C. Clarke (2003)

- Why do we simulate?
  - Cost effective
  - Fast
  - Proven method
- 
- *We cannot test!*

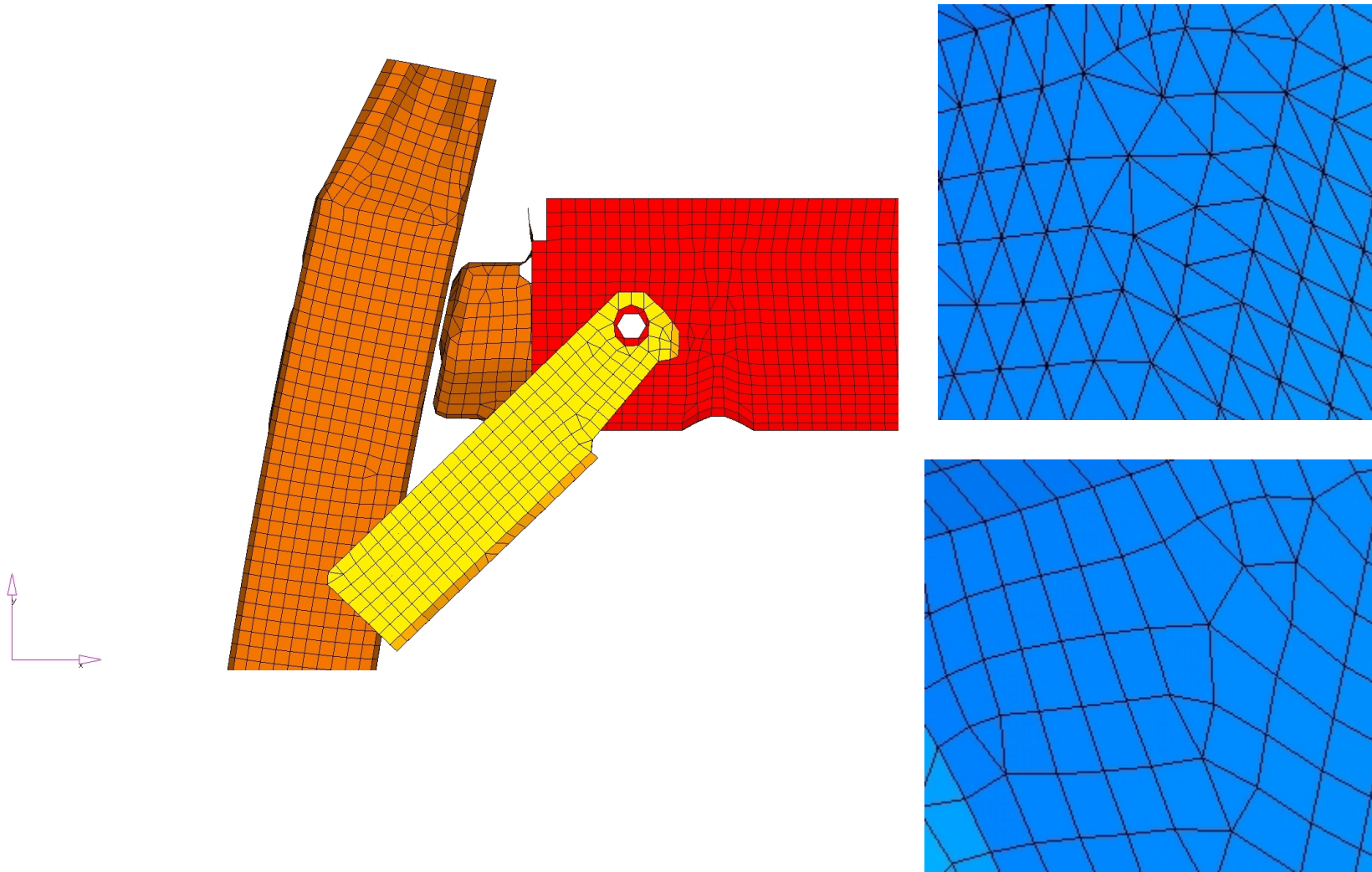




Number of Elements for a FE Crashmodel BIW



- How should a mesh look like?



## Simple box crash experiment:

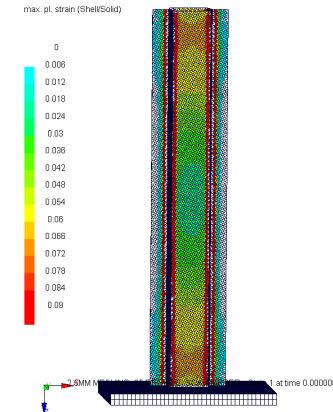
Box section 50 mm x 80 x 500mm,  $t = 1.0\text{mm}$ , mild steel

Varied parameters:

- average edge length 15/10/5/2,5mm
- mesh orientation 0deg/ 25deg
- different mesh/ integration method: Belytschko-Tsay/ Fully Integration
- Varied number of spotwelds
- With and without mapping or stamping data
- Renumbering and move in space

Objective:

- Is the result depending on the element length?
- Is the result depending on the element orientation?
- How does mapping influence/stabalise the results?
- How do small changes in the input influence the results?

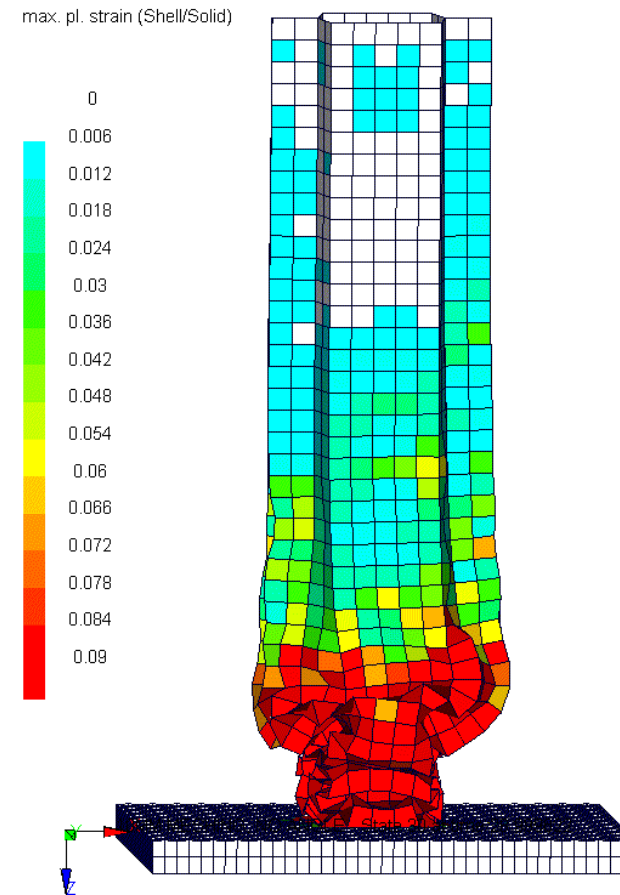
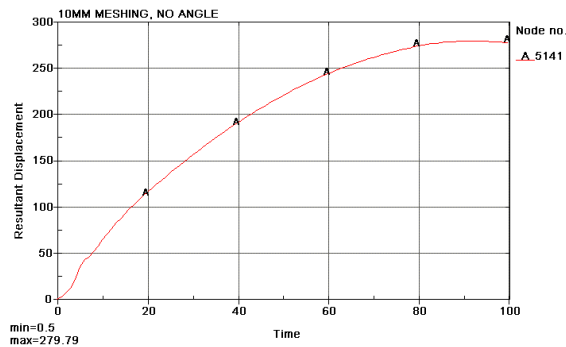
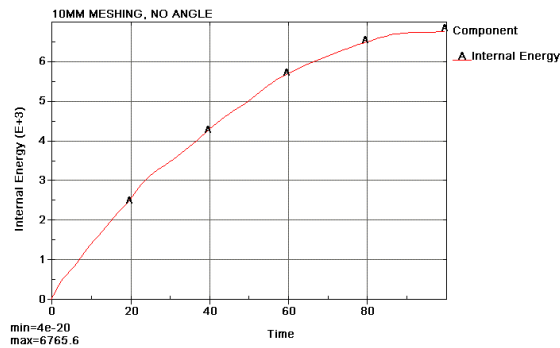


## analysis: defomation plots

v10\_1: 10mm mesh, 0deg

max internal energy 6766Nmm

max displacement 278mm

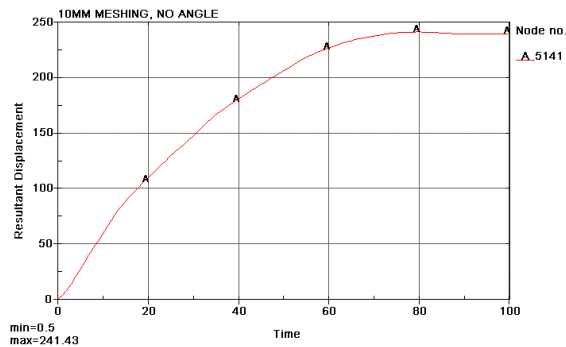
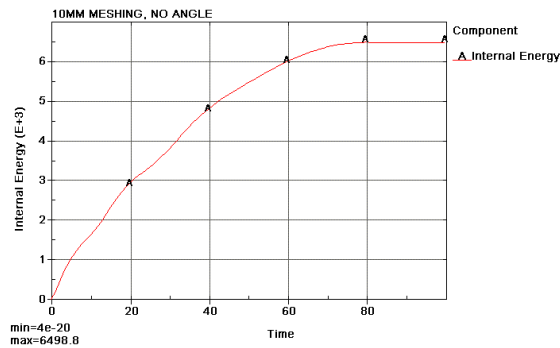


## analysis: deformation plots

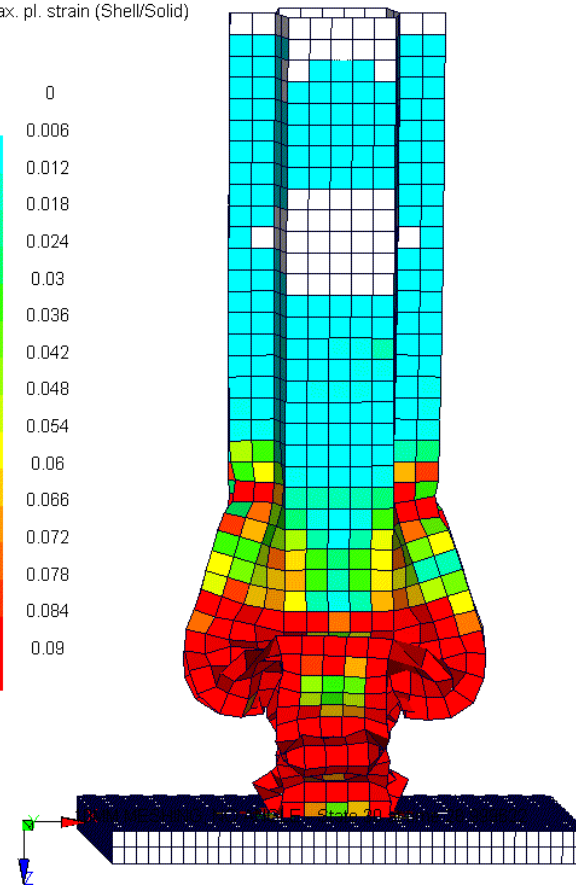
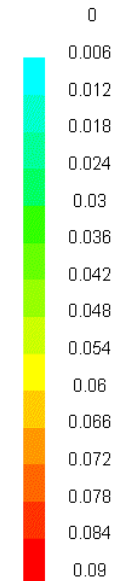
V10\_1n: 10mm mesh, 0 deg, full integration

max internal energy 6499Nmm

max displacement 241mm

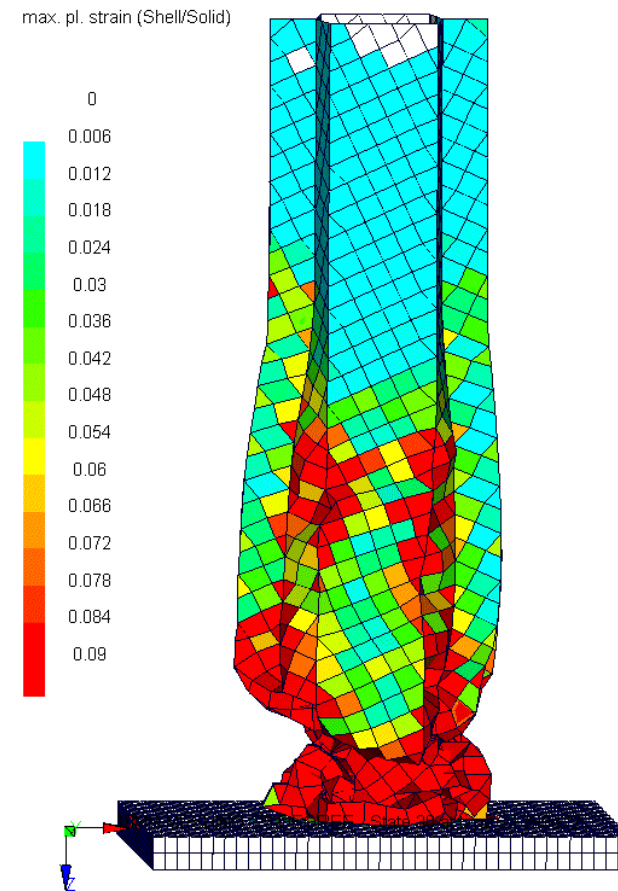
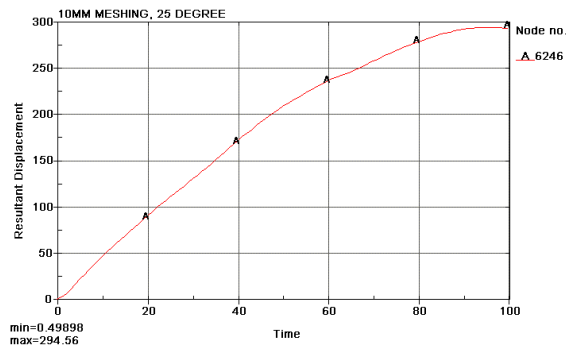
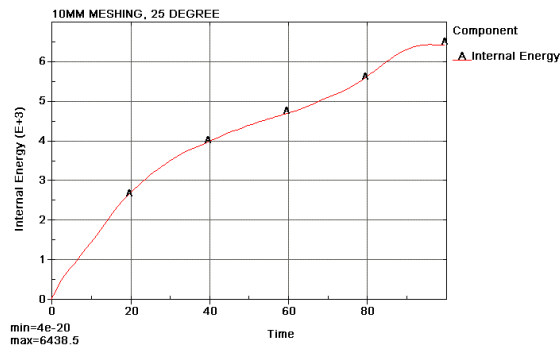


max. pl. strain (Shell/Solid)



## analysis: deformation plots

v10\_2: 10mm mesh, 25deg  
 max internal energy 6439Nmm  
 max displacement 295mm

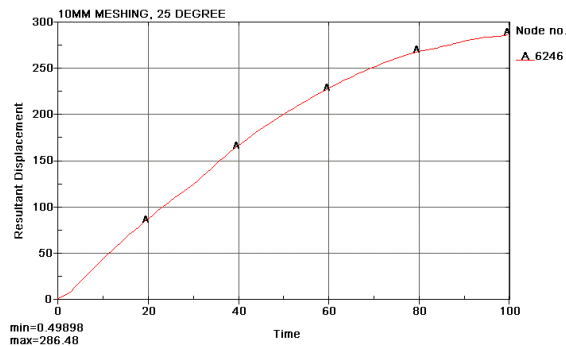
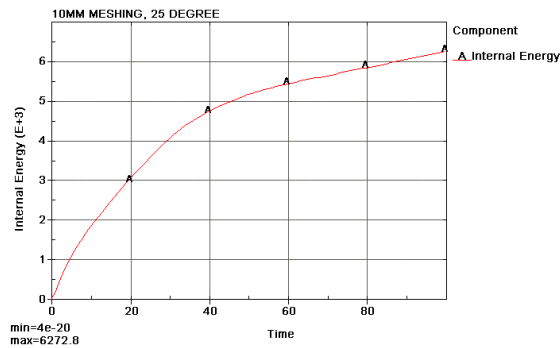


## analysis: defomation plots

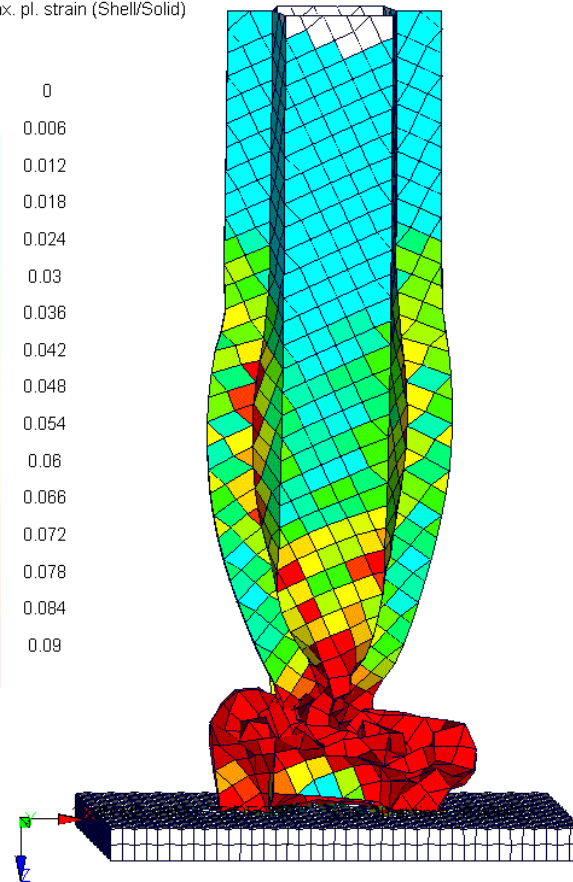
V10\_2n: 10mm mesh, 25 deg, full integration

max internal energy 6272Nmm

max displacement 286mm



max. pl. strain (Shell/Solid)

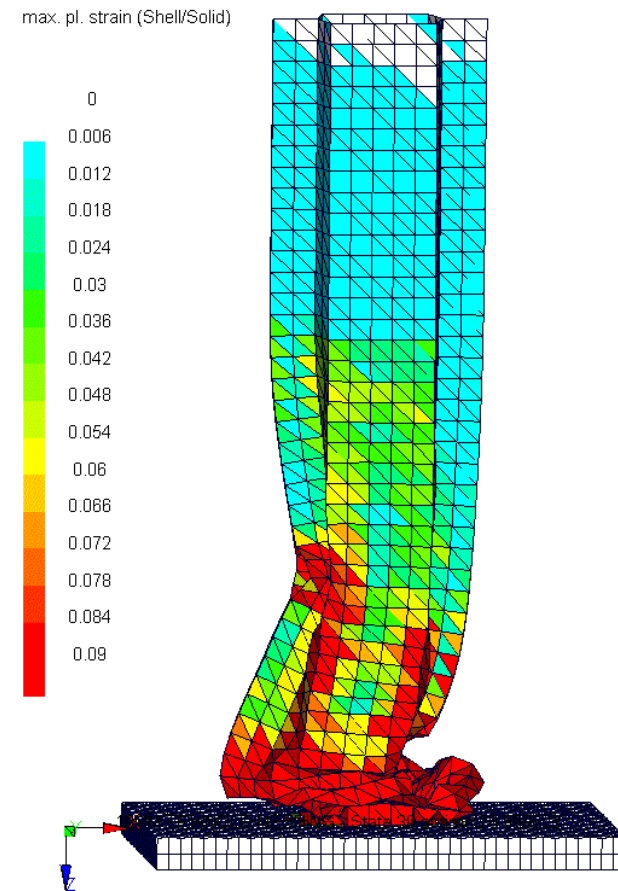
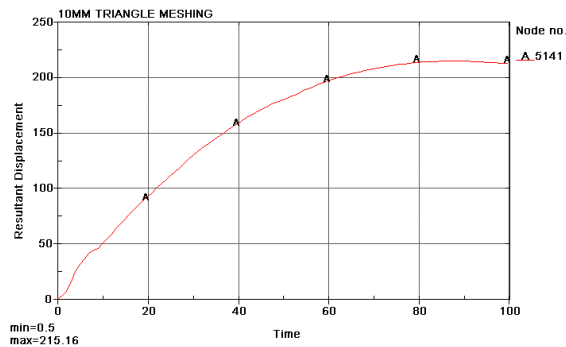
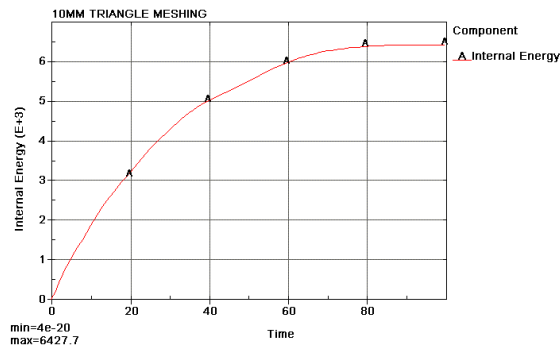


## analysis: deformation plots

v10\_3: 10mm triangle mesh

max internal energy 6428Nmm

max displacement 215mm



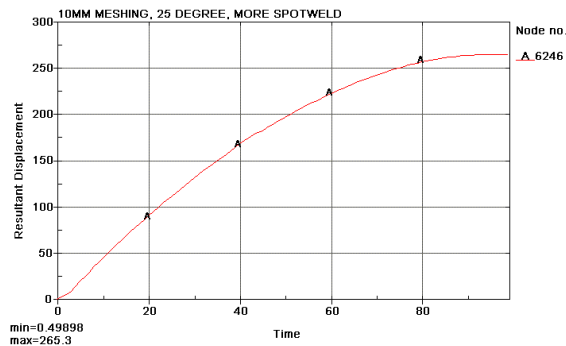
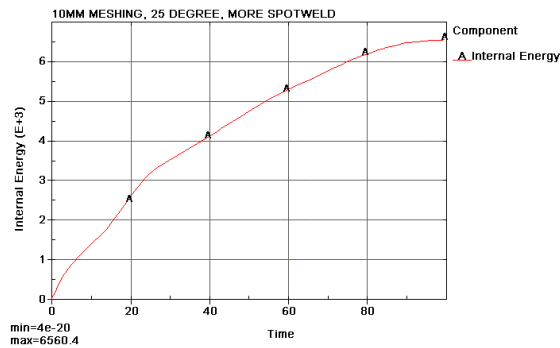


## analysis: deformation plots

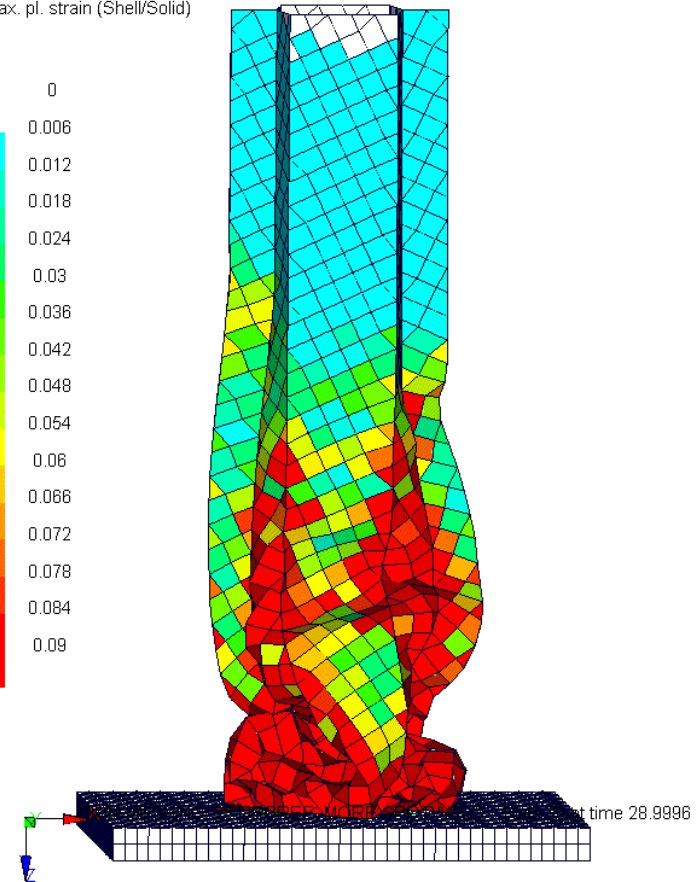
v10\_4: 10mm mesh, 25deg, more spotweld

max internal energy 6560Nmm

max displacement 265mm



max. pl. strain (Shell/Solid)

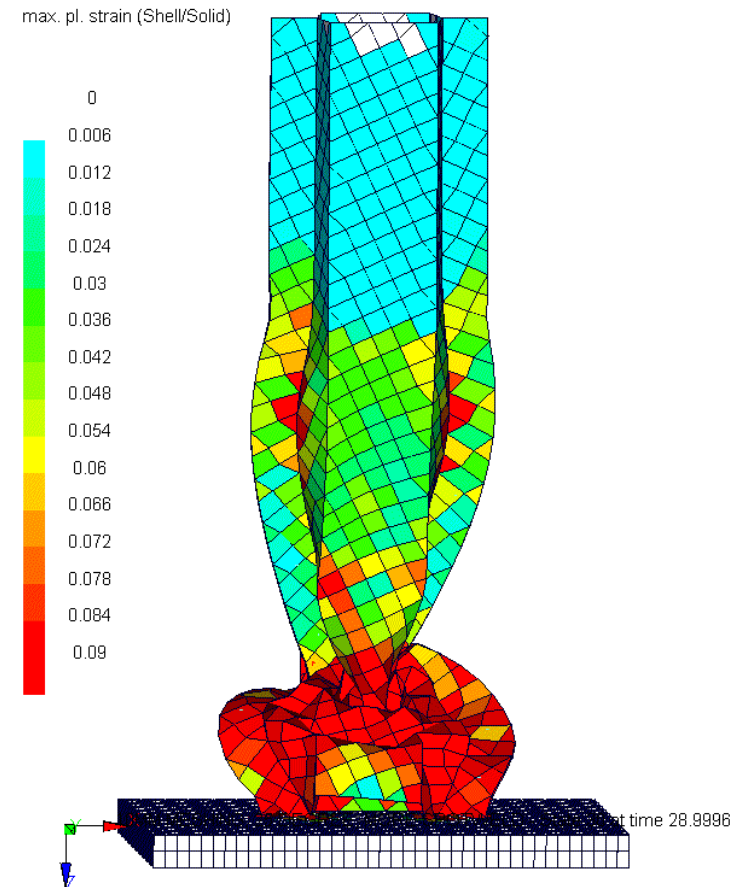
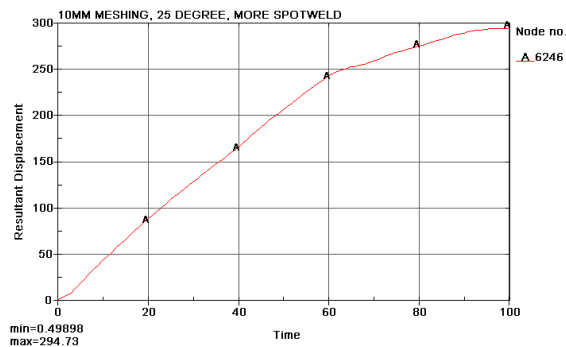
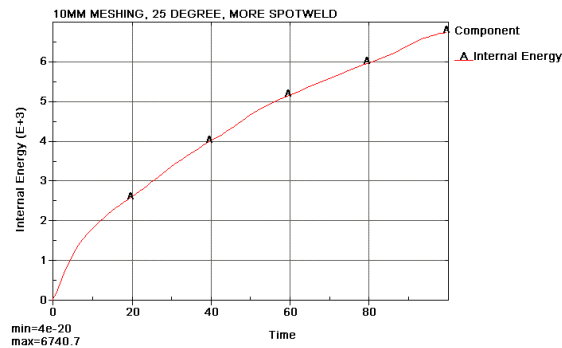


## analysis: defomation plots

V10\_4n: 10mm mesh, 25 deg, more spotweld, full integration

max internal energy 6741Nmm

max displacement 295mm

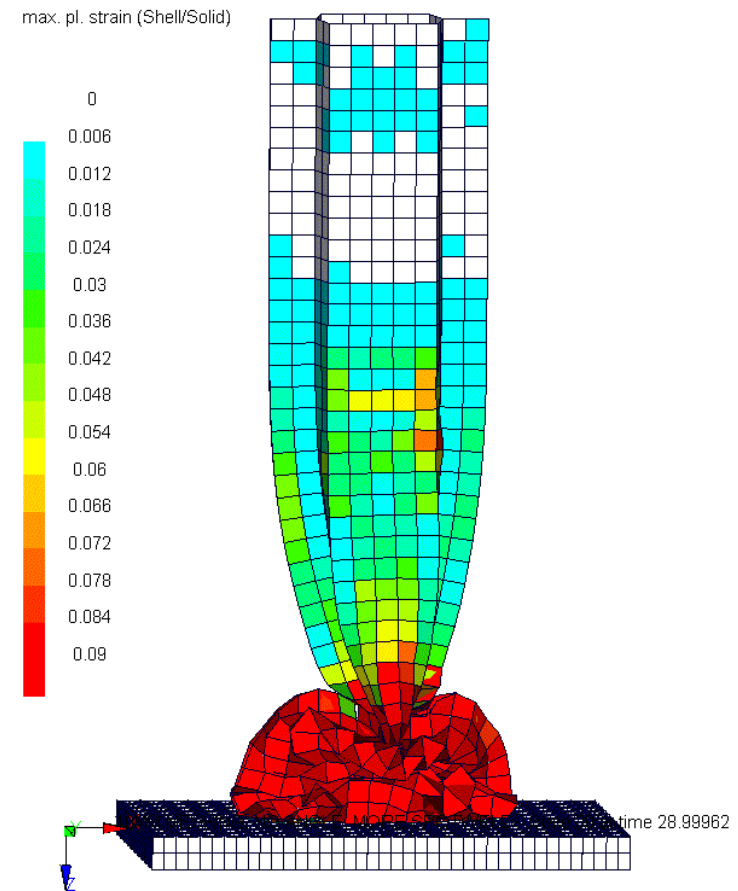
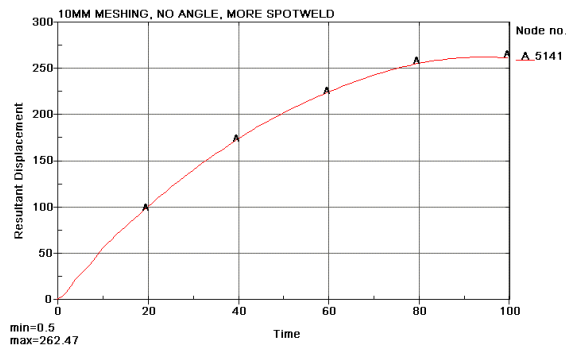
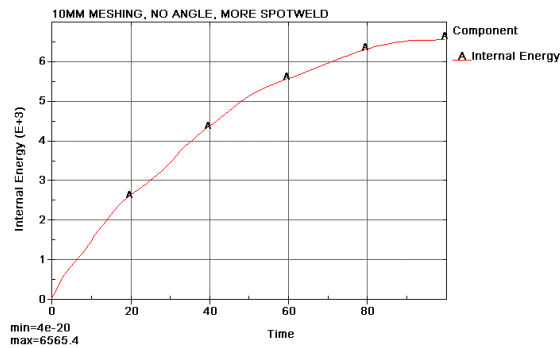


## analysis: defomation plots

v10\_5: 10mm mesh, 0 deg, more spotweld

max internal energy 6565Nmm

max displacement 262mm

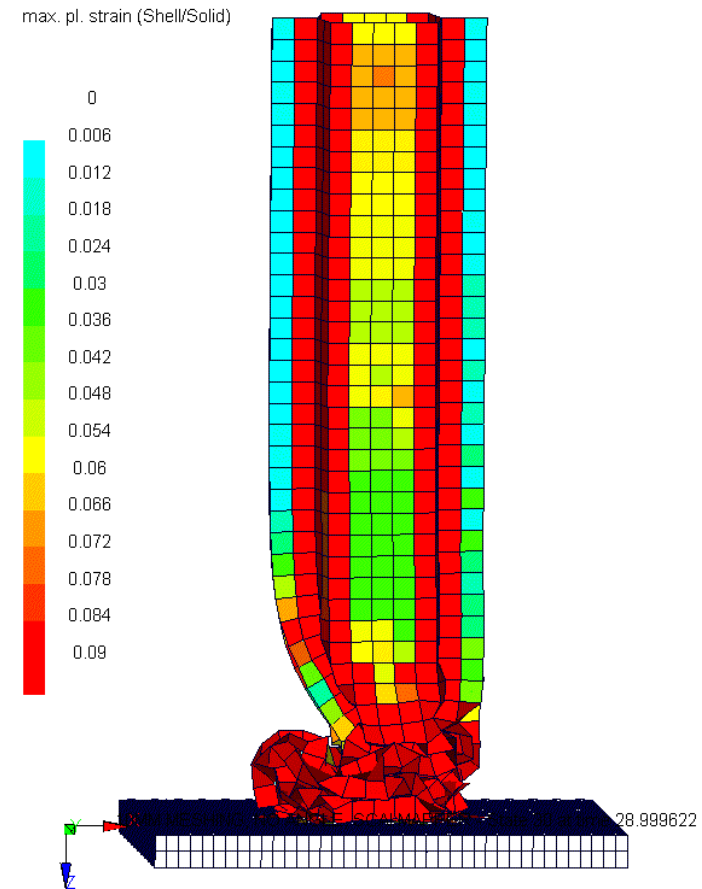
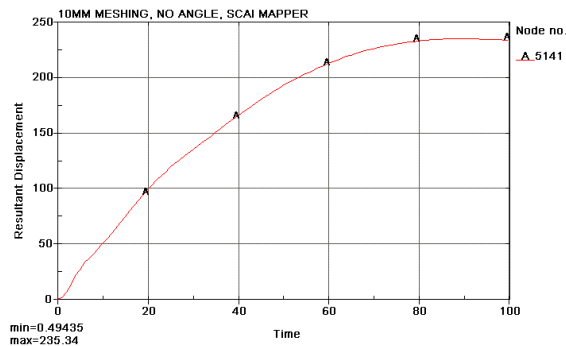
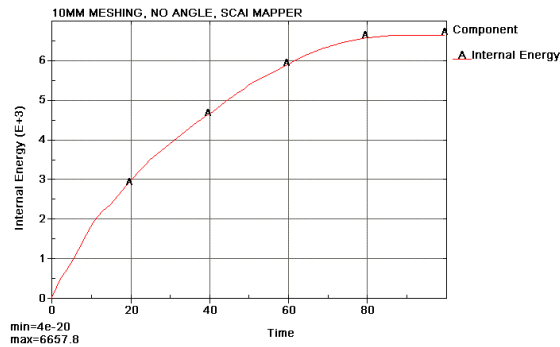


## analysis: defomation plots

v10\_6: 10mm mesh, 0deg mapped  
stamping data MpCCI

max internal energy 6658Nmm

max displacement 235mm

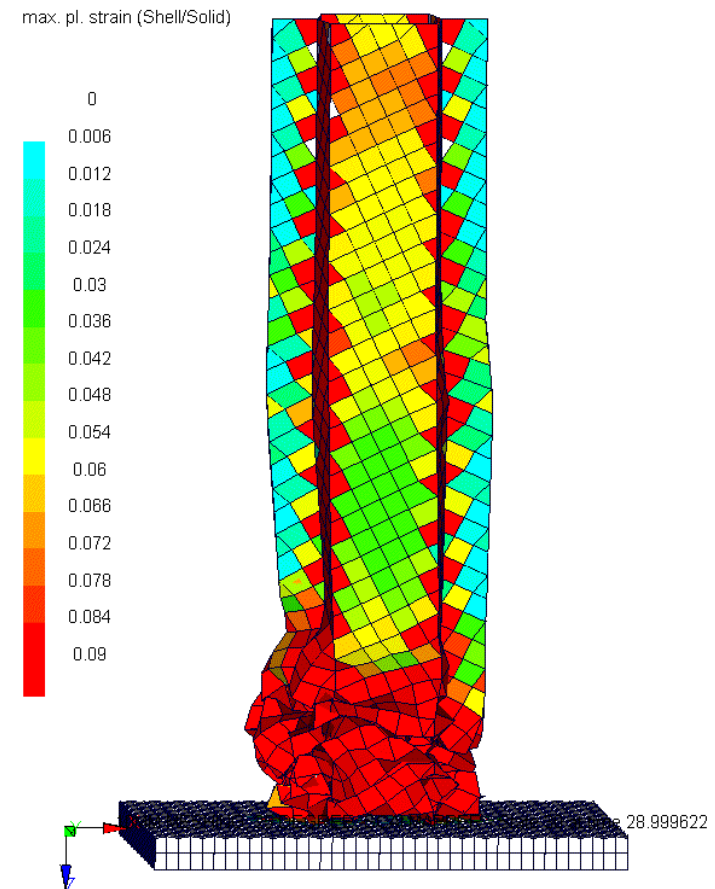
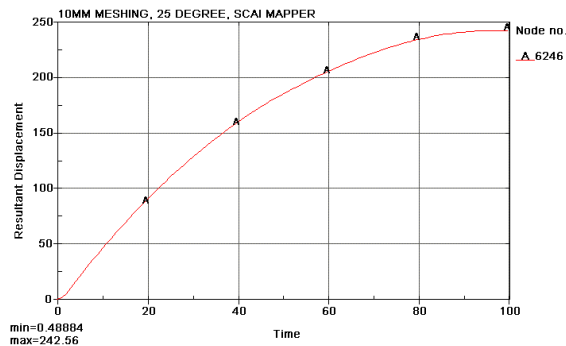
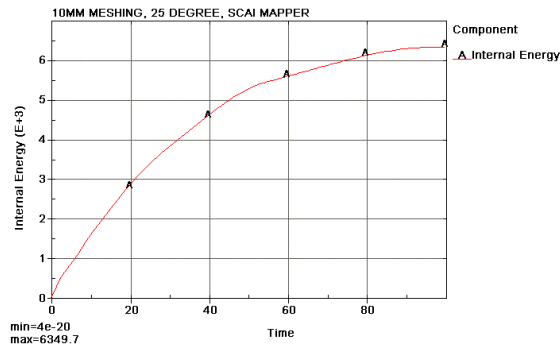


## analysis: defomation plots

v10\_7: 10mm mesh, 25deg mapped  
stamping data MpCCI

max internal energy 6350Nmm

max displacement 243mm

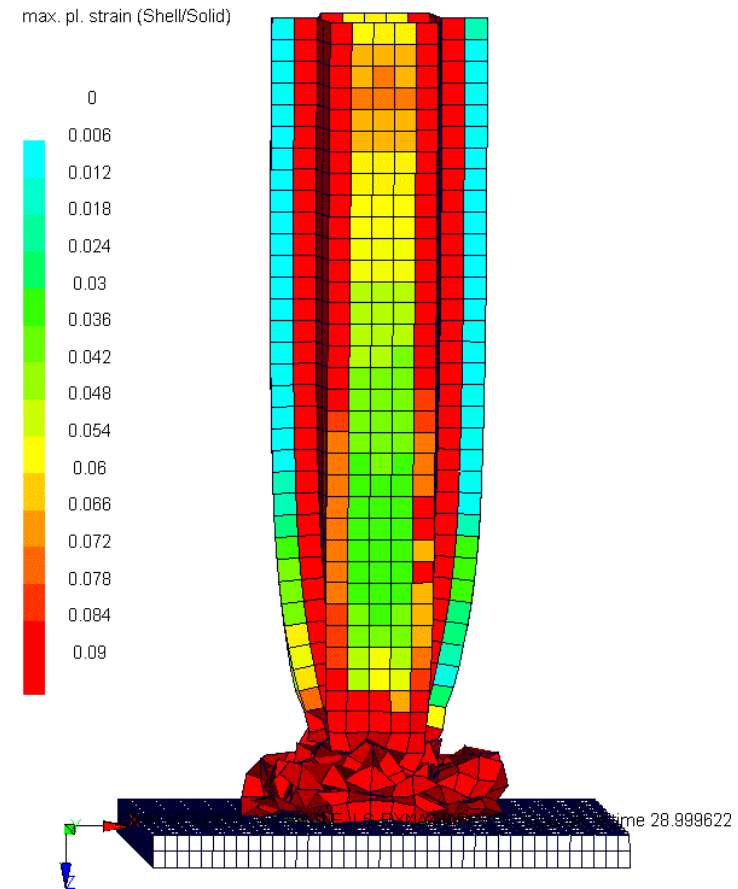
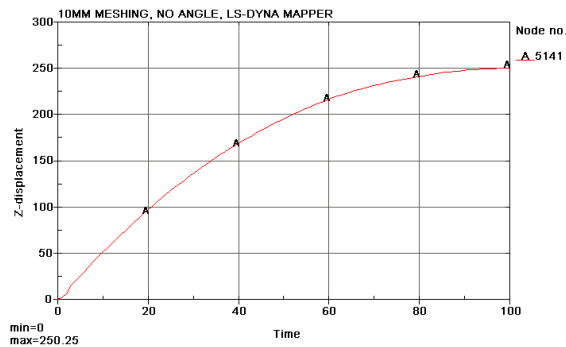
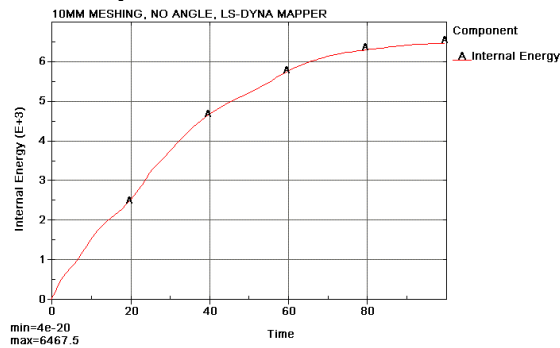


## analysis: defomation plots

v10\_6n: 10mm mesh, 0deg mapped  
stamping data DYNAIN

max internal energy 6468Nmm

max displacement 250mm

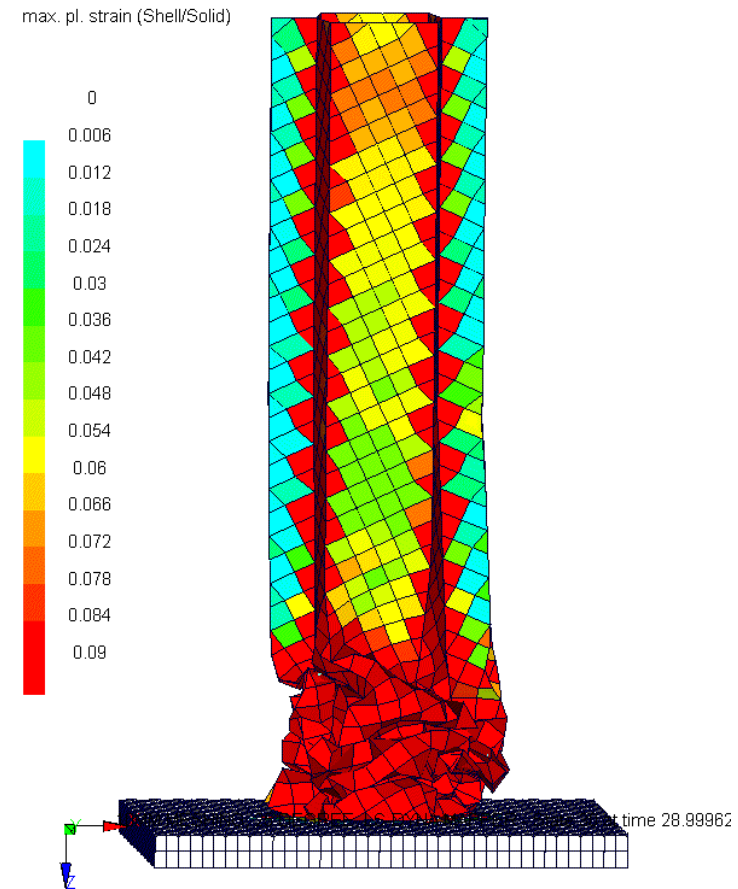
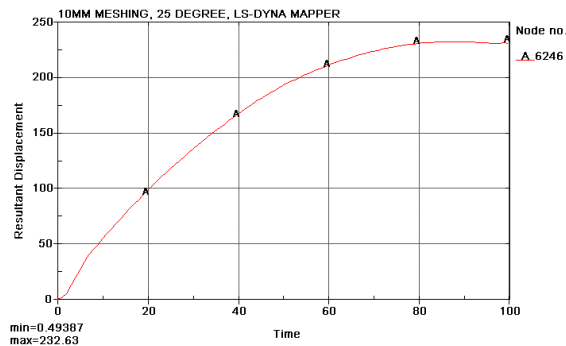
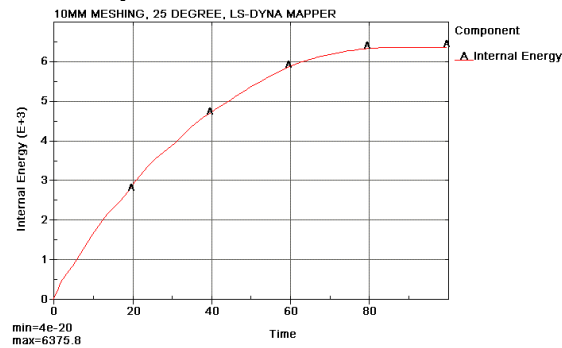


## analysis: defomation plots

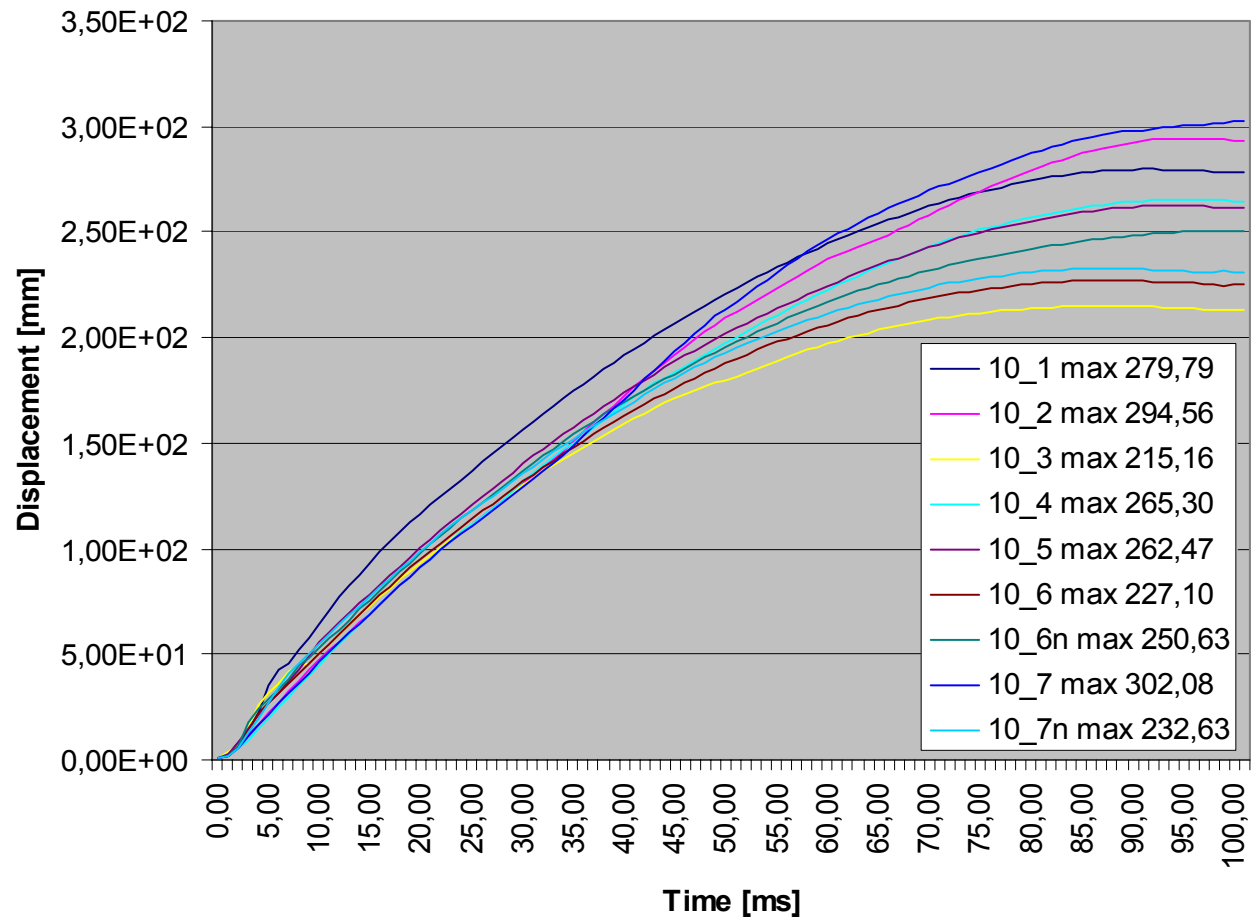
v10\_7n: 10mm mesh, 25deg mapped  
stamping data DYNAIN

max internal energy 6376Nmm

max displacement 233mm



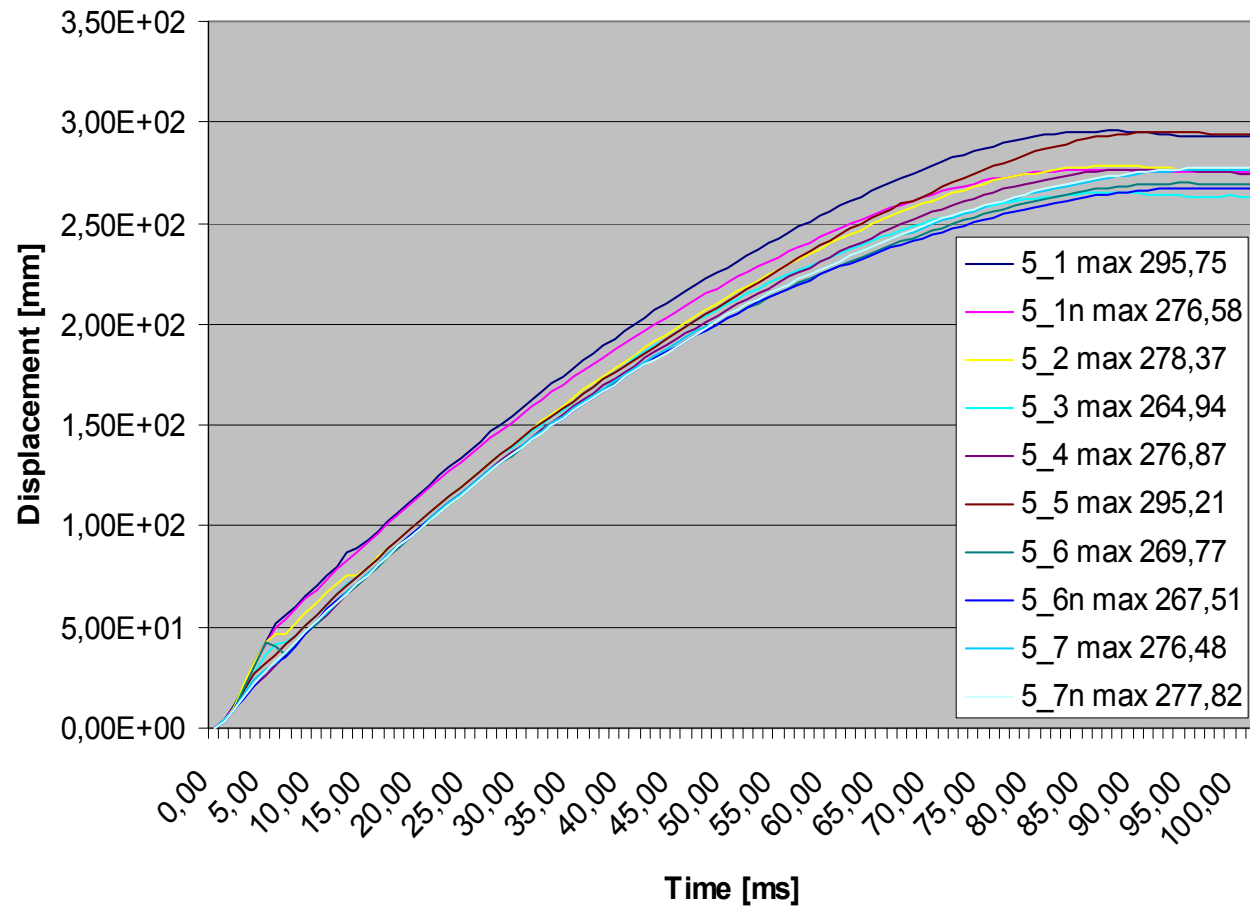
## Analysis: comparison of Displacement 10mm meshing



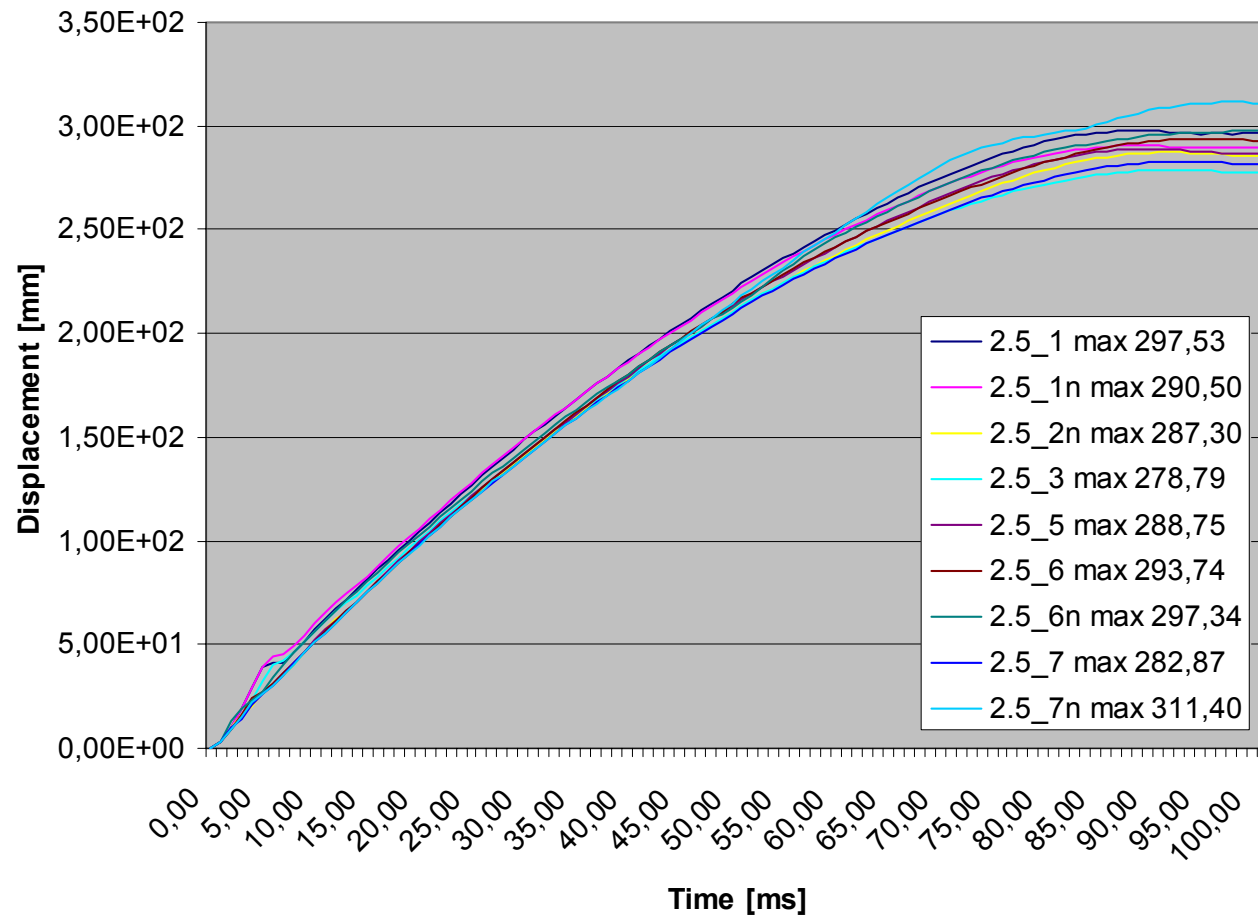


## Analysis: comparison of Displacement

5mm meshing

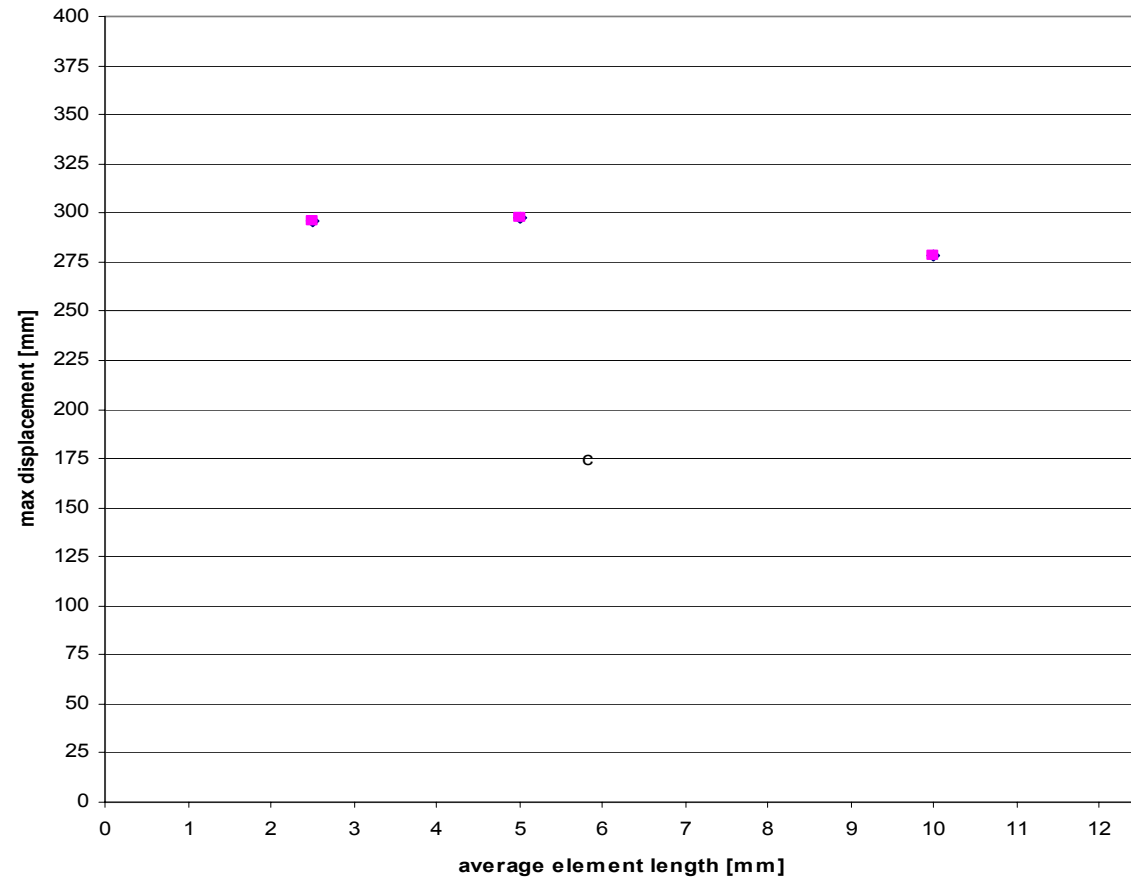


## Analysis: comparison of Displacement 2.5mm meshing



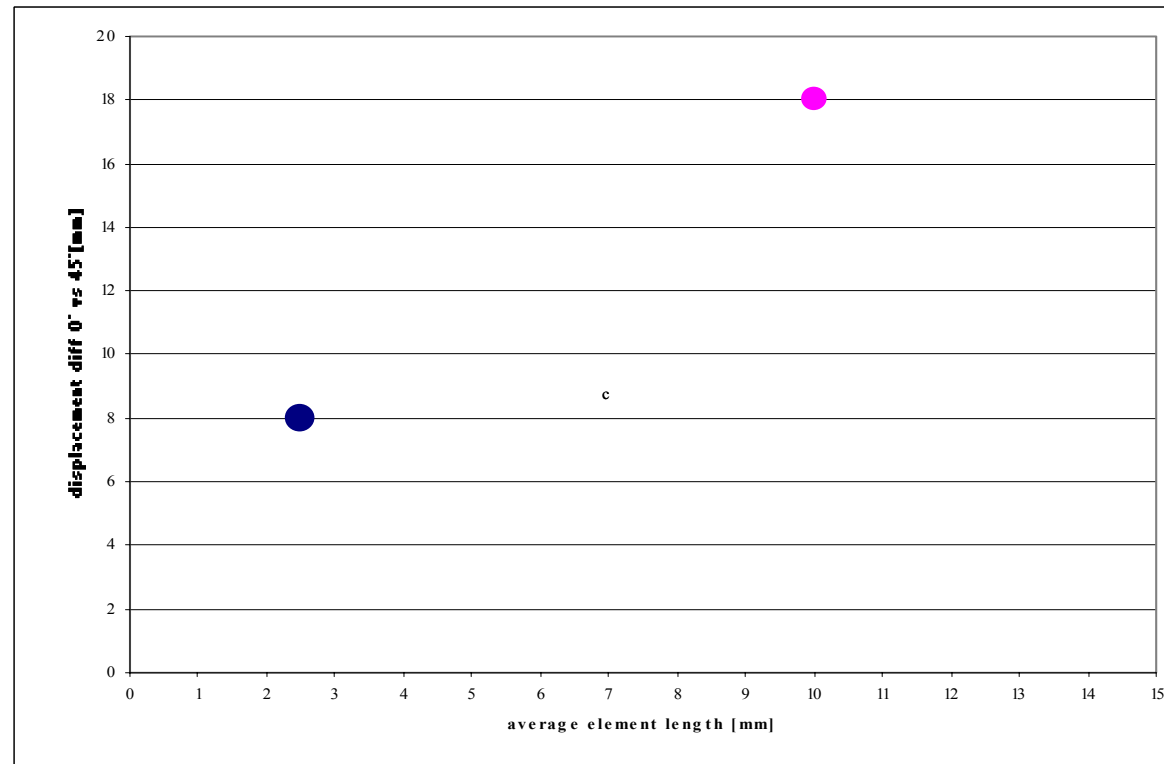
## Analysis: Comparison max. displacement

Compression is nearly independent from the element length in a range from 10mm to 2.5 mm for the same element orientation



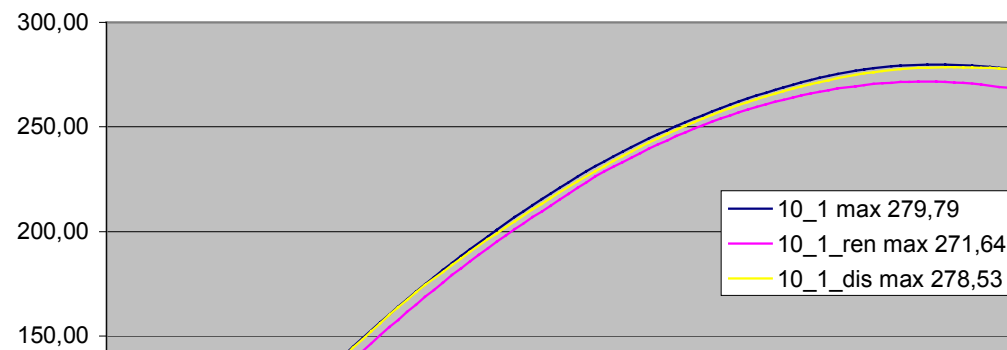
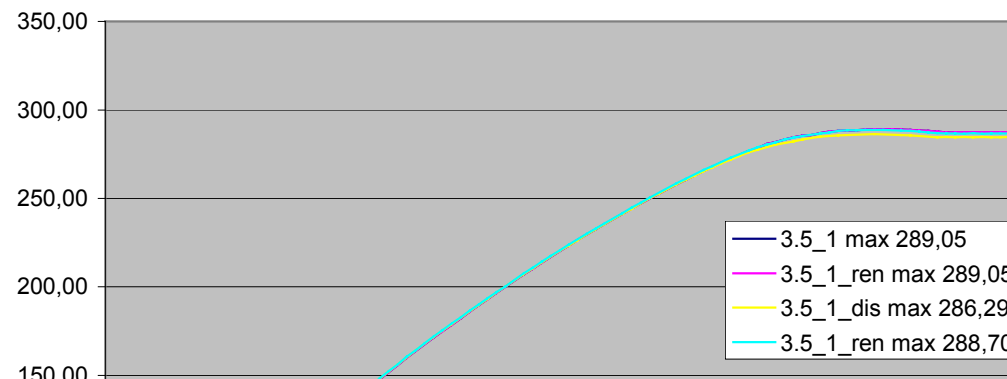
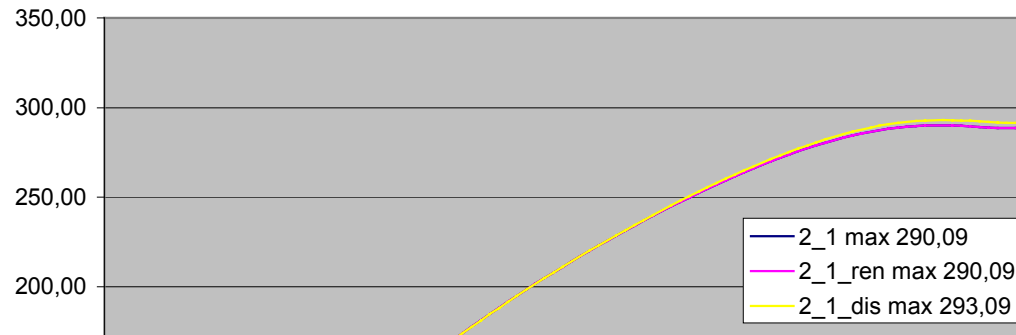
## Analysis: Comparison max. displacement

The max displacement difference for 0° mesh and 25° mesh is small for finer meshes and big for coarser meshes



## Analysis: Influence on mesh translation and renumbering

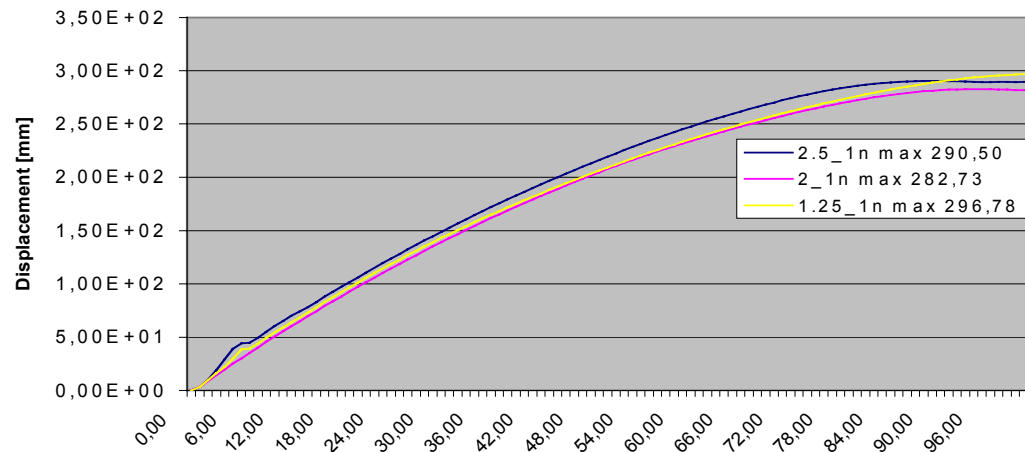
For 10 mm the variation is about 8mm where as the deviation for smaller elements sizes is about 3mm for the same element orientation



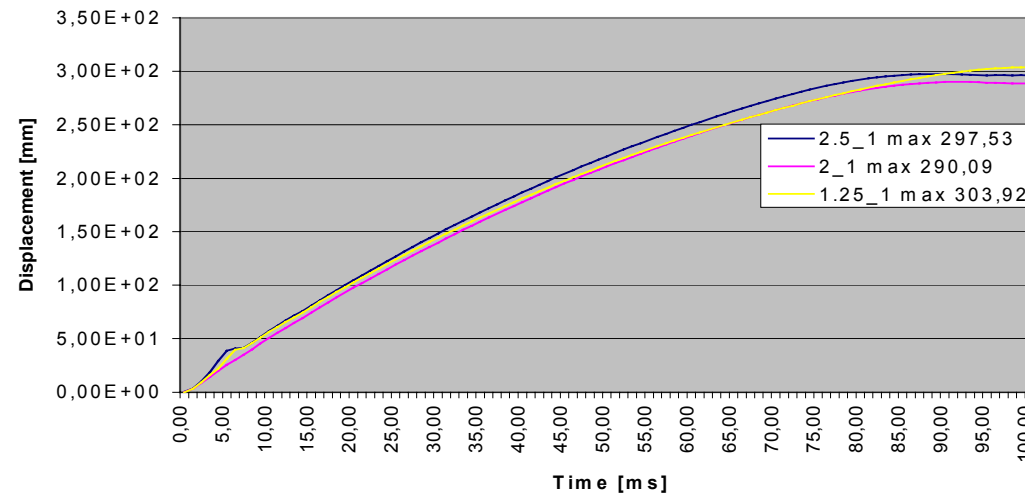
## Analysis: Influence on results of very small elements.

For 1,25 mm the BT (typ2) element seems to be too weak. For smaller elements sizes, full integration seems to have better results.

Comparison of Full Integration

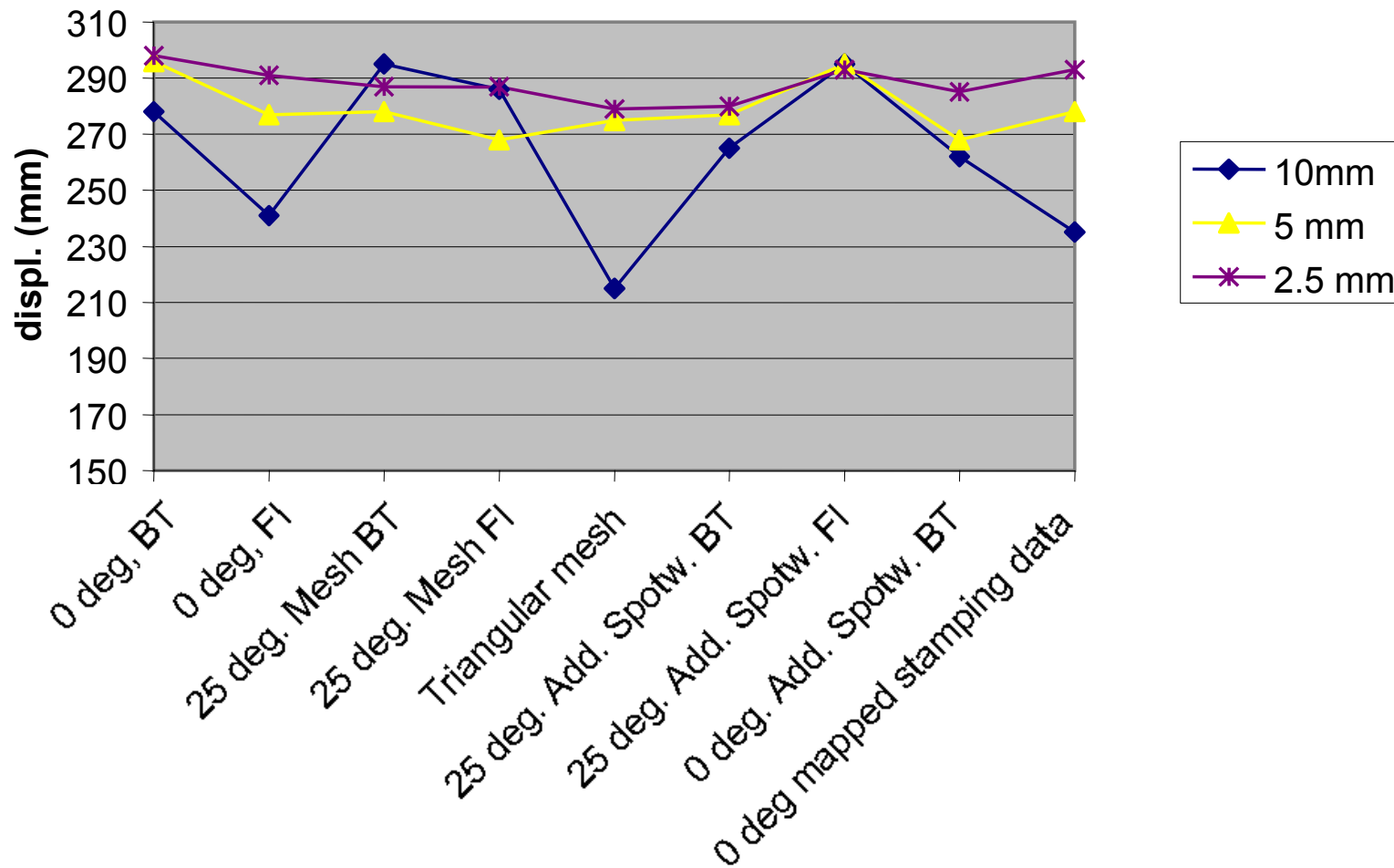


Comparison of BT



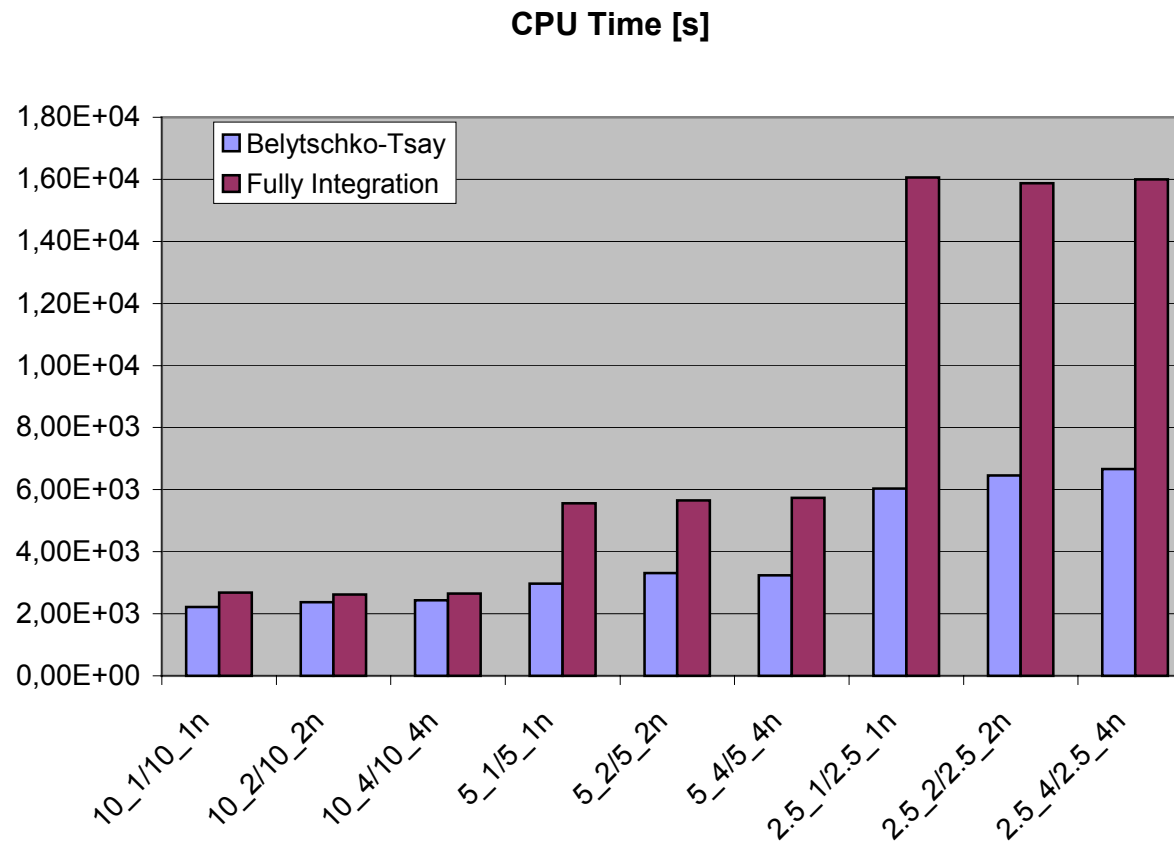
# Analysis: comparison max displacement variation

variation for different mesh sizes



## Analysis: Comparison of integration method

Calculation Time





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### **Results**

- Results for the displacement and the internal energy seem to be smooth and stable in a range from 15mm to 2,5 mm for orthogonal element orientation
- Different element orientation give different results for coarser meshes
- Finer mesh is not so sensitive for different element orientation, integration method, number of spotwelds, mapping, small changes in the input (renumbering, moving the model in space)
- Mapping tools are easy to use for Crash coupling. The influence of the mapping was getting smaller for smaller element sizes for the influenced zone was getting smaller and the crash mode was very stable in our example.

### Conclusion

- If you know the collapse mode of a part you can use a coarse mesh which should be orthogonal in the collapse direction (so you can achieve “superconvergence”)
  - If you doesn't know the collapse mode of a part; Please use finer meshes
  - No one knows the exact collapse mode of all the parts in a vehicle!
  - Meshing rules for orthogonal /Mapping/Integration schemes meshes are important for coarser meshes but not important for finer meshes.
- 
- *Creation of finer meshes can be automated by TEC ODM!*

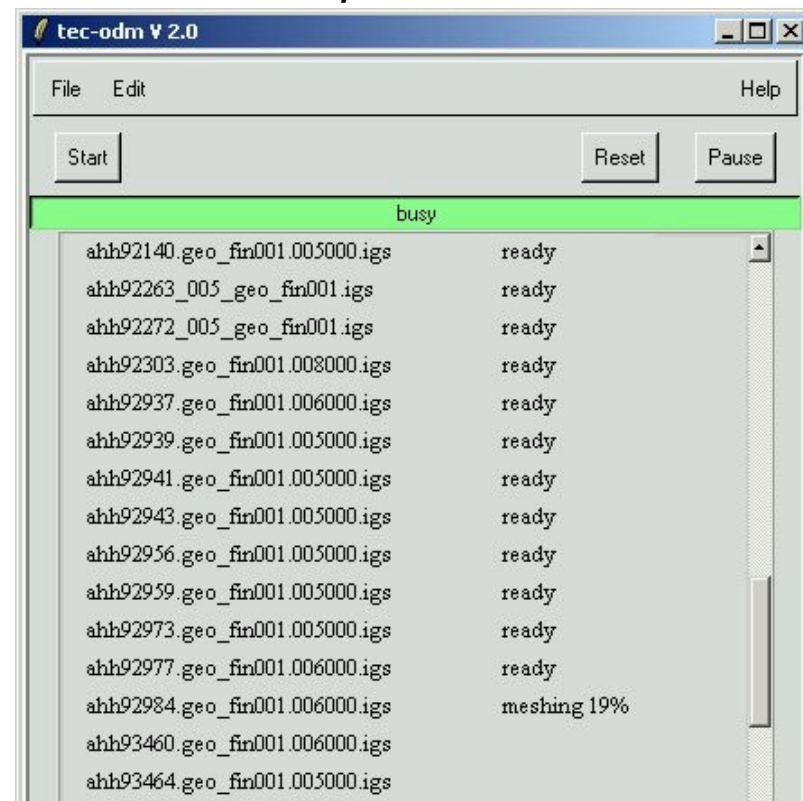
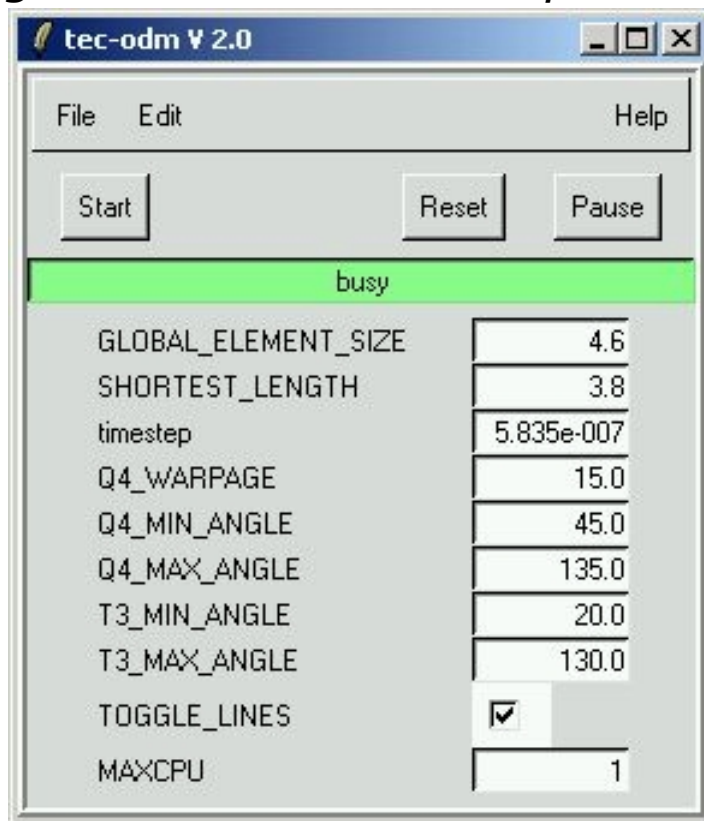
- What is TEC-ODM?
- What can TEC-ODM do?
- How can the development process benefit from TEC-ODM?
- What is the System requirement

# Automatic Meshing Pro's and Con's



- What is TEC-ODM?

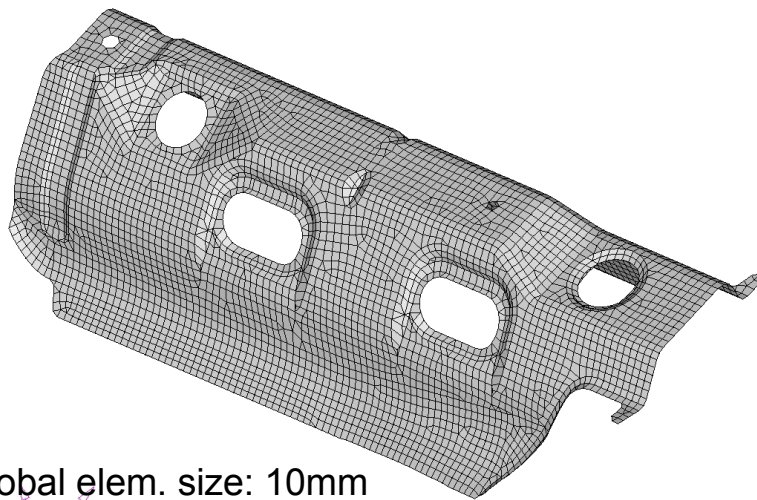
- *Tec ODM (One Day Meshing) is a automatic FE batch meshing Software for Body in White meshes for Crash and NVH analysis. Tec ODM is based on a set of 50 different explicit mesh enhancement algorithms which are implemented in iterative loops.*



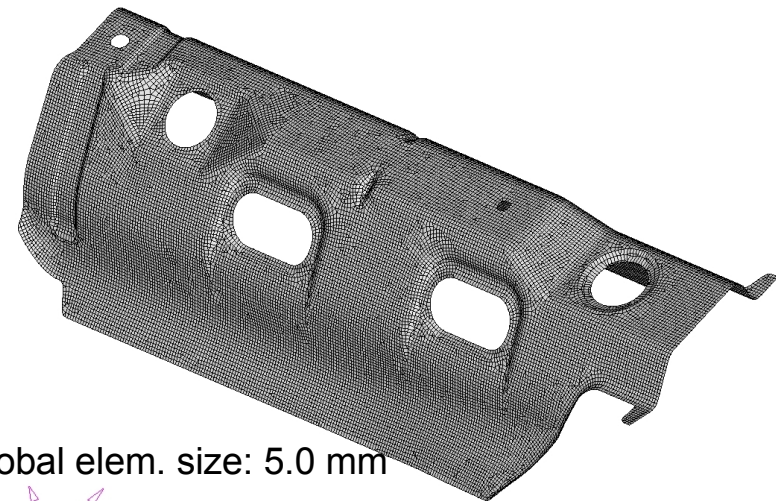
## Automatic Meshing Pro's and Con's



- What can TEC-ODM do?
  - *Tec ODM creates FE shell element meshes on CAD surfaces considering different quality criteria. TEC ODM's output is a mesh with distinguished global element sizes (11 mm or smaller) and smallest element length up to 4.0 mm.*



Global elem. size: 10mm  
Smallest elem. Size: 4.0 mm



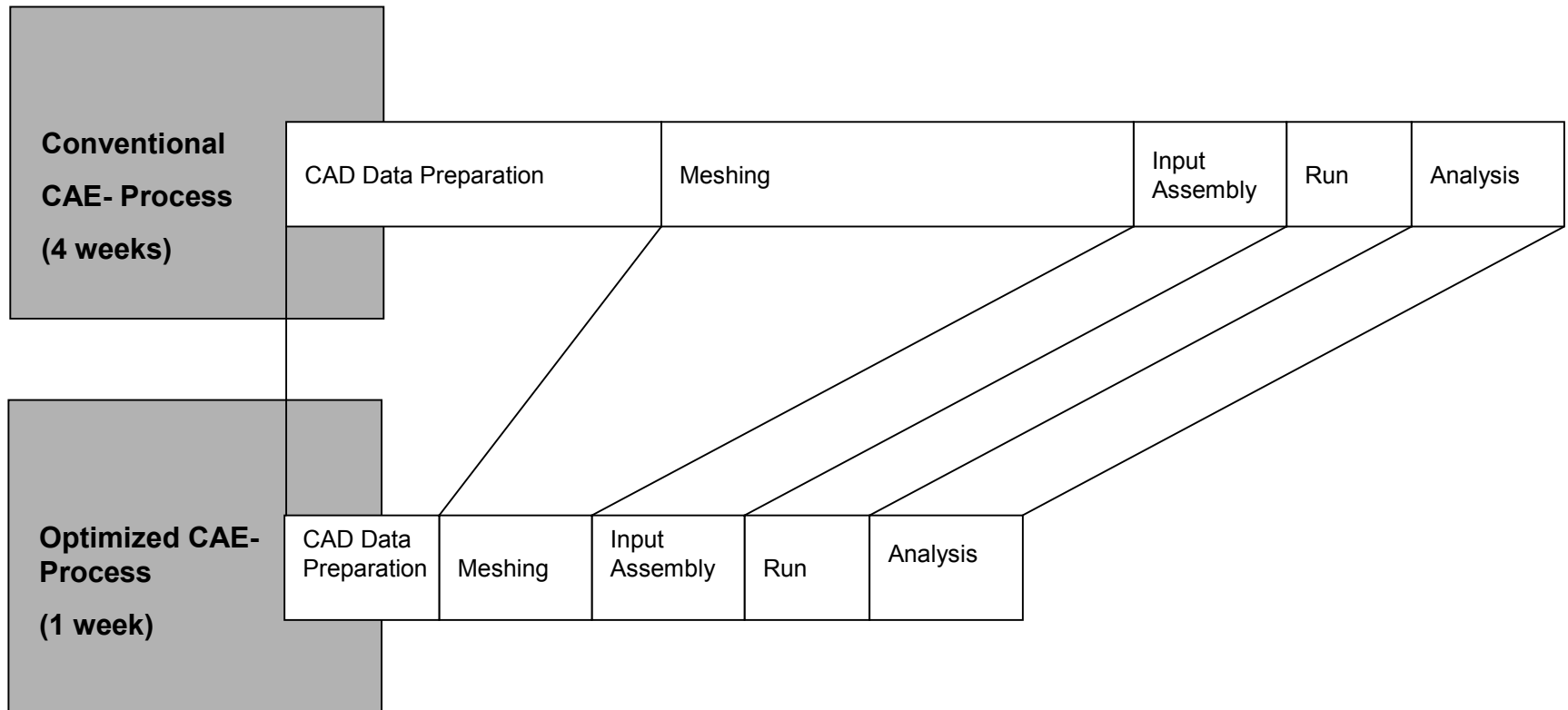
Global elem. size: 5.0 mm  
Smallest elem. Size: 3.0 mm

# Automatic Meshing Pro's and Con's



- How can the development Process benefit from TEC ODM?

Time saving through CAE- Process Optimisation  
earlier results



# Automatic Meshing Pro's and Con's



- How can the development Process benefit from TEC ODM?

**Cost saving through CAE- Process Optimisation**

	Regular FE Process	TEC ODM Process
Additional Software cost for a MPP license	0 €	149.000 €
Cost for an BIW FE Mesh outsourced from CAE supplier	40.000 €	0 €
Number of updates per Year per Platform	5	5
Number of platforms @ car manufacturer	10	10
Total cost for BIW FE mesh per year	2.000.000 €	149.000 €
Investment needed for additional Hardware eg. Linux Cluster with 192 Processors		€ 288.000
Manpower/ inhouse cost for TEC ODM operation (50 days for 50 BIW FE Mesh update)		€ 30.000
Total cost	2.000.000 €	467.000 €
Possible savings with TEC ODM per year		<b>1.533.000 €</b>

# Automatic Meshing Pro's and Con's



**Manual Mesh**

**ODM mesh**

	Number of elements		Number of elements	
	complete model	804819	complete model	1922676

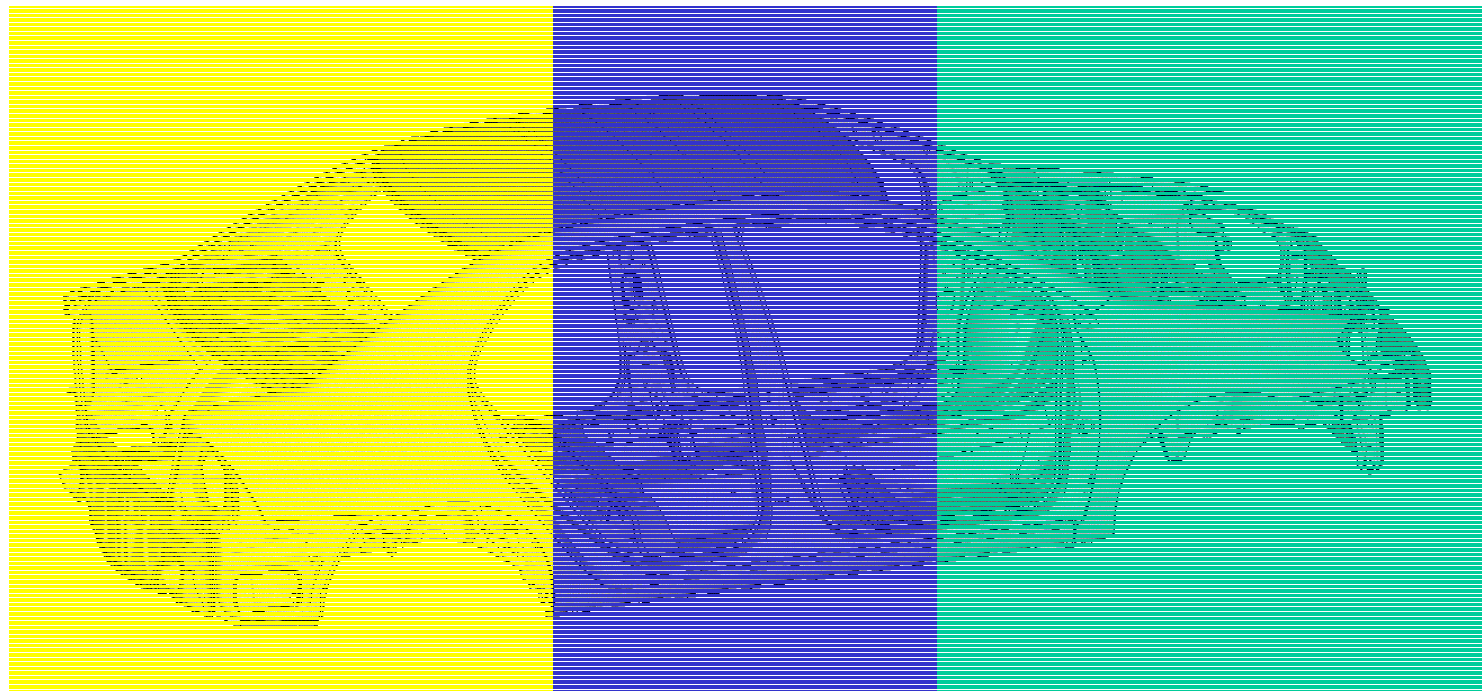
***„Model size is getting bigger with TEC ODM therefore some investment in numbercrunching is needed.***



# Automatic Meshing Pro's and Con's



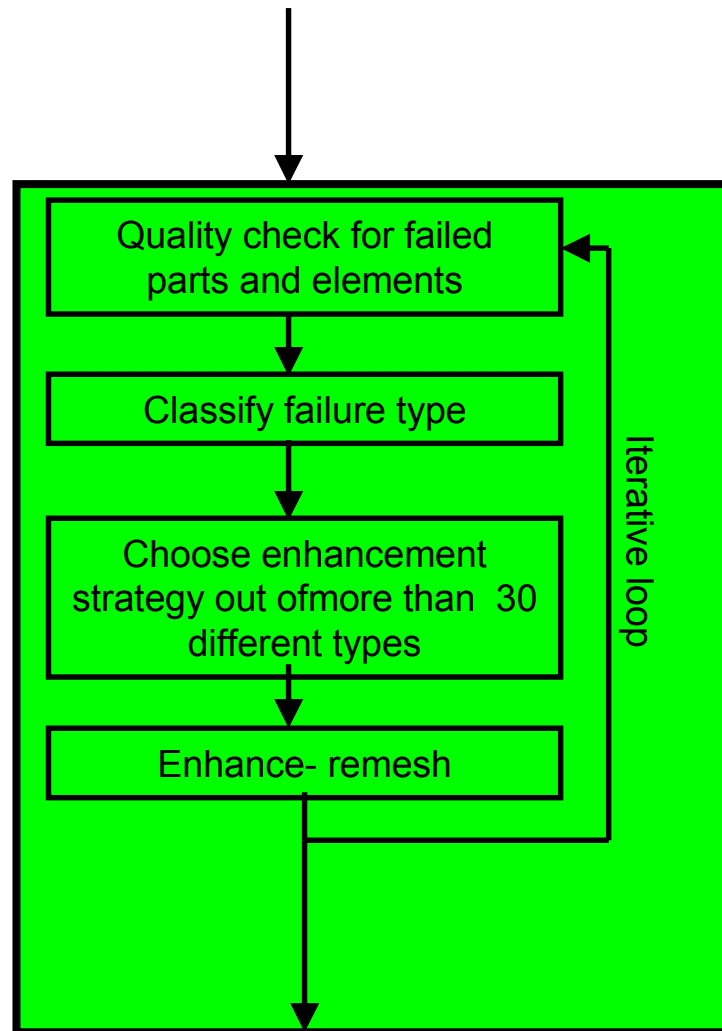
- *Ways of using TEC ODM*



15-20 mm

6-12 mm

3-6 mm



- TEC ODM automesh process is ready to use
- TEC ODM will result in bigger FE models
- ODM process will result in faster answers to engineering questions and reduced modelling cost
- TEC ODM has nearly no “human influence” in the modelling process
- Meshing engineer becomes a quality and process checker

- Thank you!
  
- Any questions?